



cfms

COMITÉ FRANÇAIS DE MÉCANIQUE
DES SOLS ET DE GÉOTECHNIQUE

Webinaire « Doctorants en géotechnique »

Clouage des sols : comportement sous sollicitation
sismique de l'interface sol-clou



Université
Gustave
Eiffel

LABORATOIRE RRO
RISQUE ROCHEUX ET
OUVRAGES GÉOTECHNIQUES

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9 JANVIER 2024

Who are We?

RRO Test deals with applied research issues identified in particular during expertise on real projects or works.

Scope of Action:

- Observation and monitoring of sites and geotechnical structures in full scale.
- Behavior ,dimensioning, and design of geotechnical structures.

Methods of Research:

- Experimental testing (scale 1:1 or on site as possible).
- Analytical (calculations).
- Numerical approaches (CESAR-LCPC,OPTUM CE...).

On-going Research:

- Ground-frame friction for the foundations of the bolt and nail type.
- Seismic behavior of ground reinforcements by nailing.
- Behavior, design and dimensioning of the structures for protection against rockfall,
- Vulnerability of civil engineering structures required by a hard impact at moderate speed.
- Behavior and diagnosis of masonry works.
- High-precision instrumentation for monitoring works and sites by optical fiber.



Rocks fall station in Montagnole



Dynamic nail pull-out device

Soil Nailed Walls:

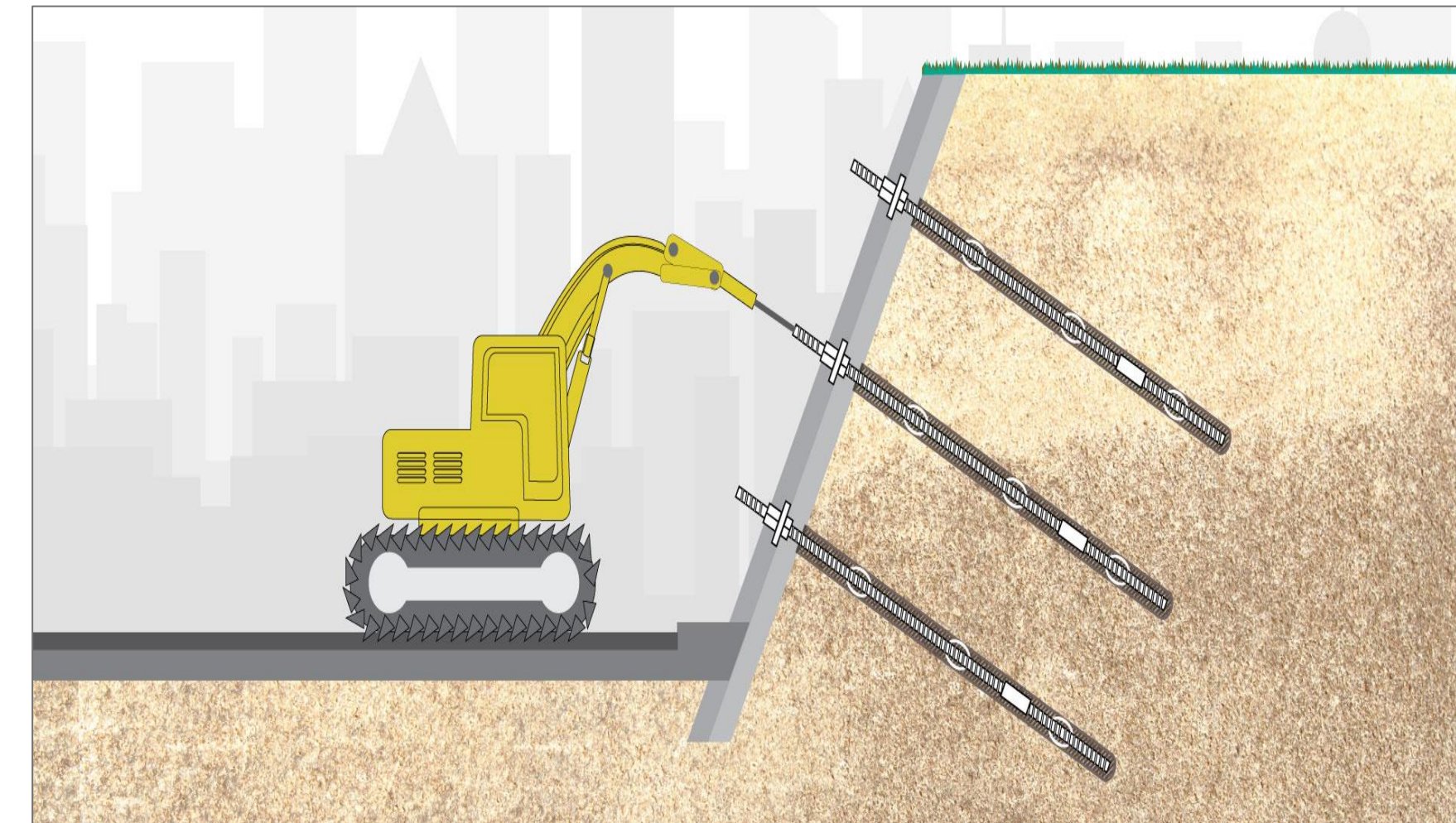
- Soil retaining structures where soil is reinforced by sealed grouted steel bars.

Economically:

- Reduced cost
- Rapid construction
- Easy implementation

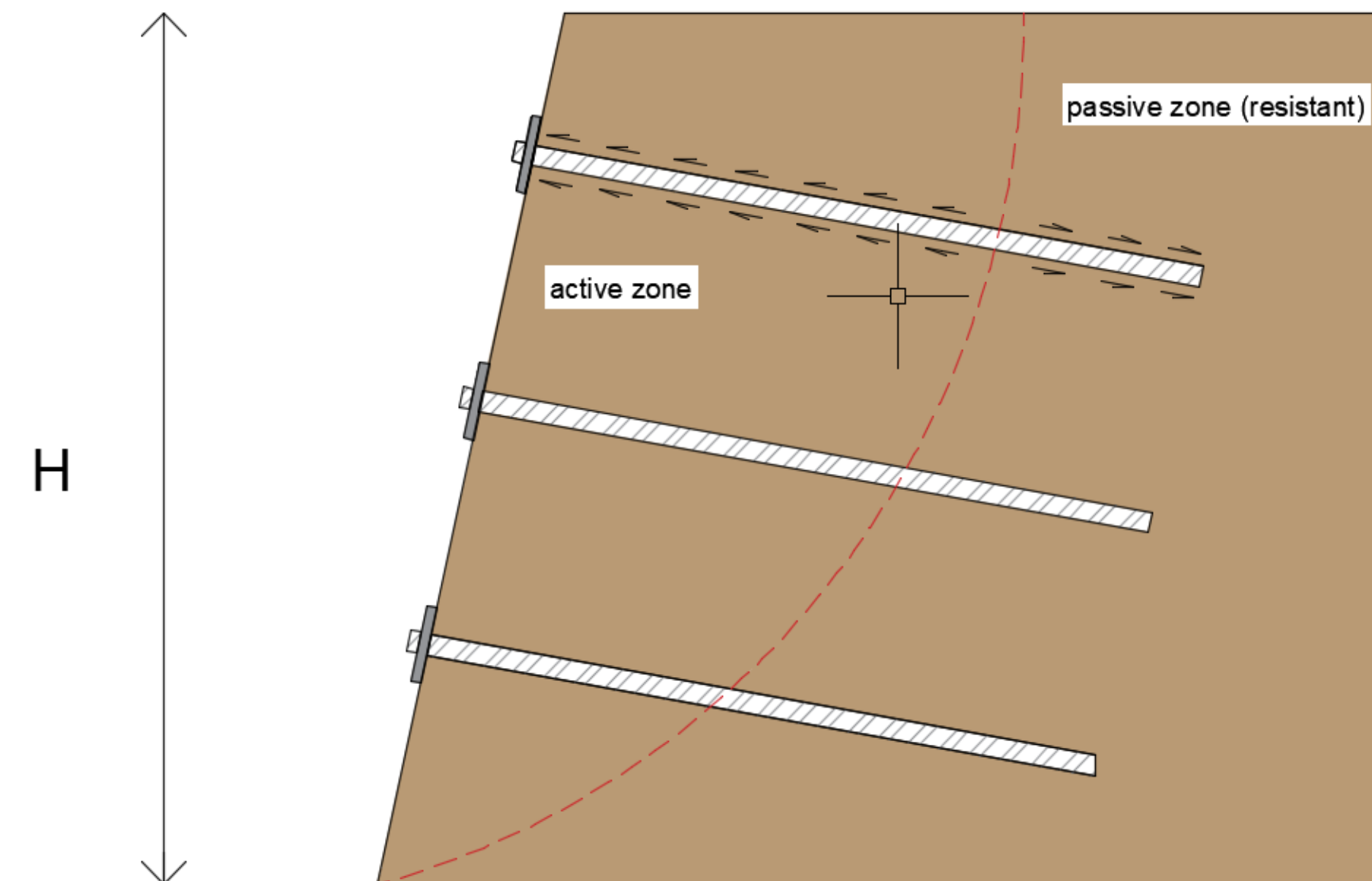
Performance:

- Remarkable seismic performance.

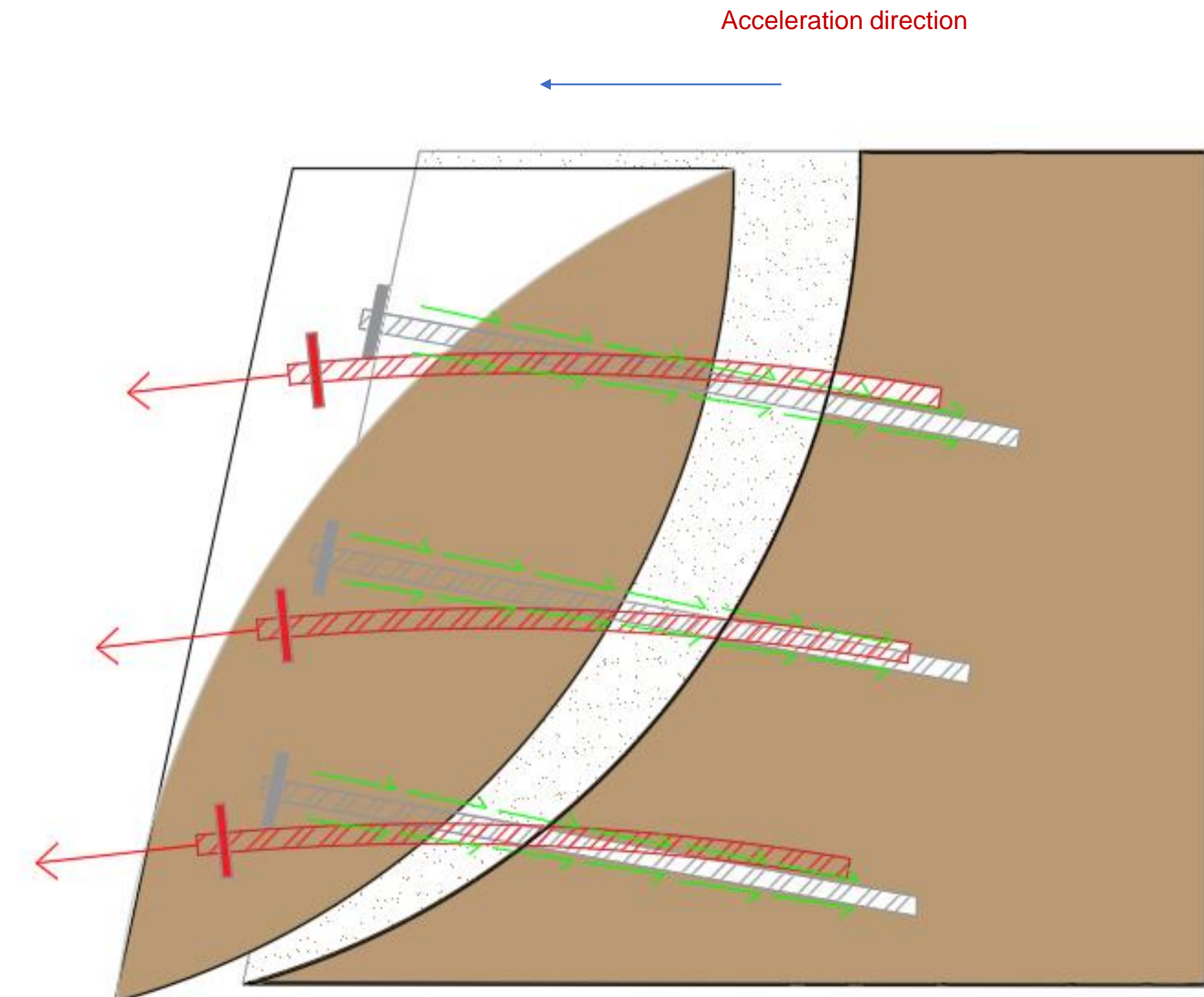


soil nail walls construction

Stability of Soil Nailed Walls:



Stability of soil-nailed walls



failure of soil-nailed walls by pull out of nails

Stability of Soil Nailed Walls: local behavior

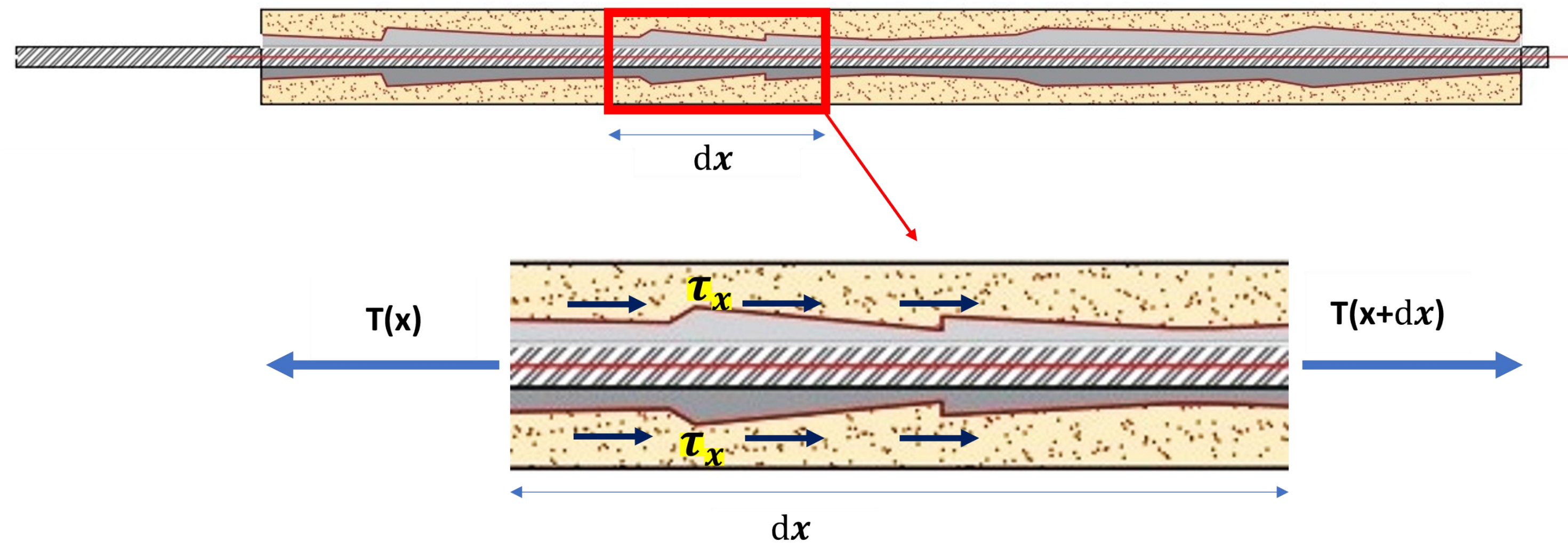
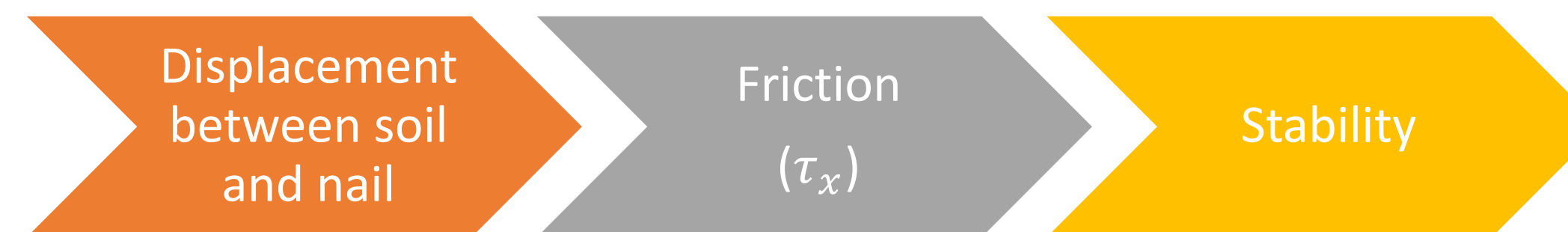
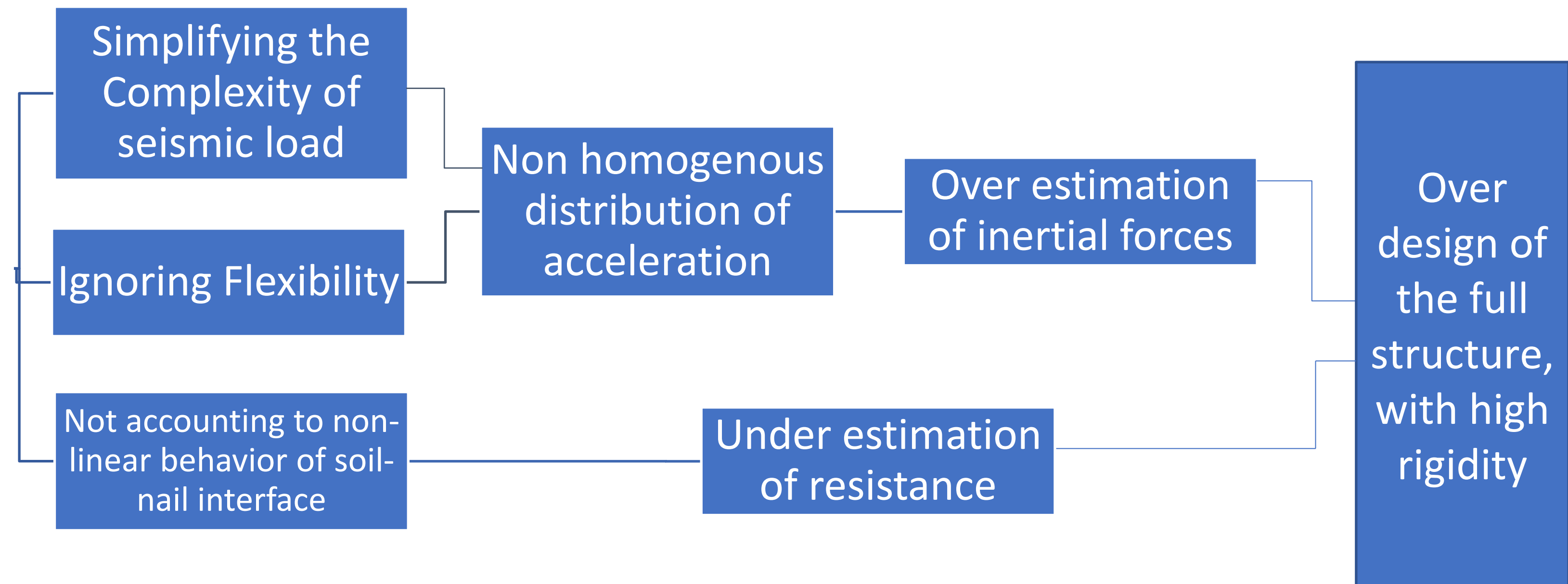


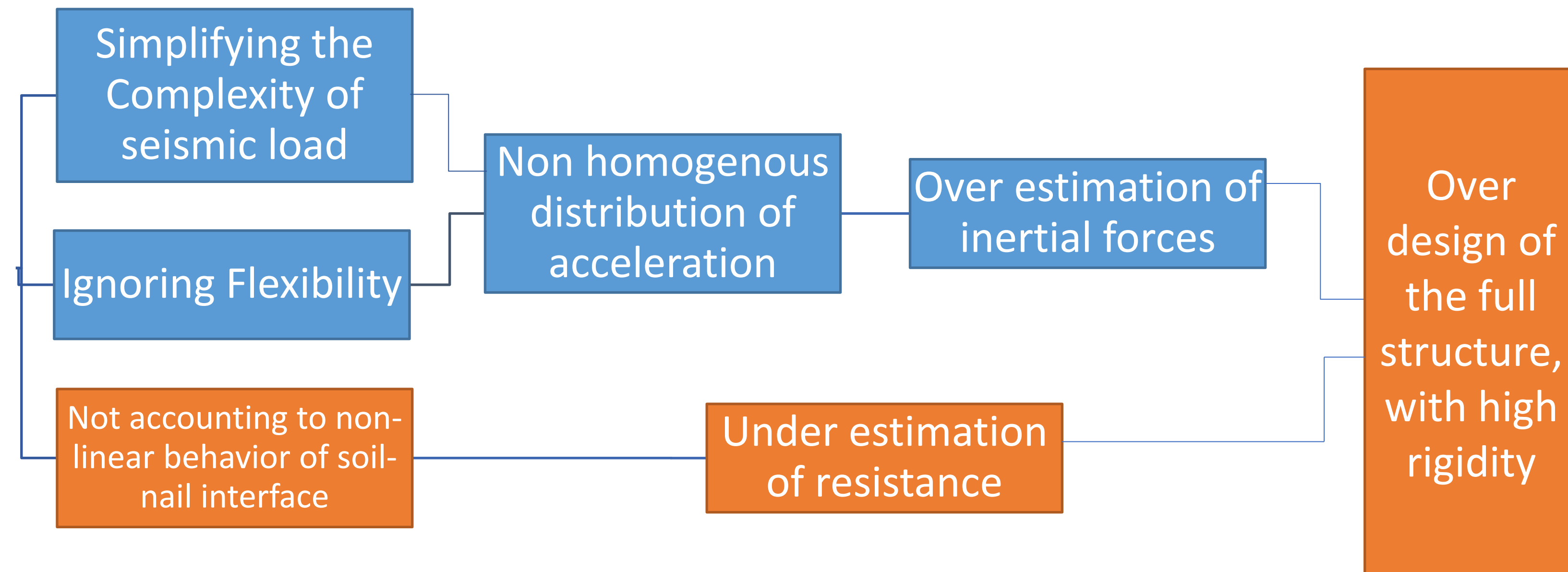
Illustration of soil-nail interface friction



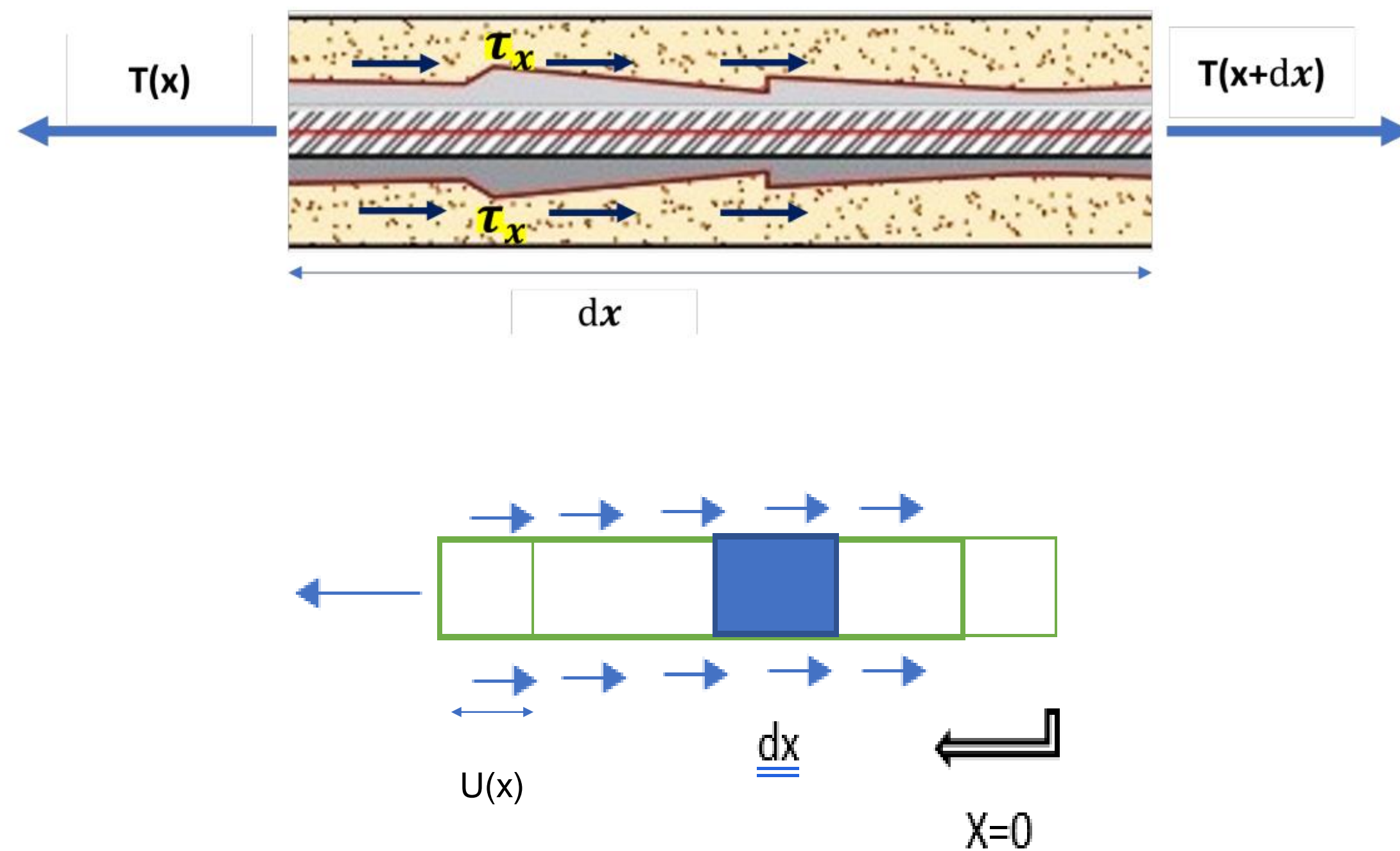
Seismic Behavior: limits of design methods



Seismic Behavior: limits of design methods



The Interface Behavior: static problem



At equilibrium:

$$T(x) - T(x + \Delta x) - \pi\tau_x D = 0$$

And according to Hook's law:

$$\sigma = E\varepsilon$$

$$\frac{dT_x}{S} = E \frac{du}{dx}$$

The equations add up to form a 2nd order differential equation:

$$ES \frac{d^2U}{dx^2} - \pi\tau_x D = 0$$

$$\frac{d^2U}{dx^2} = \frac{\pi\tau_x D}{ES}$$

The Interface Behavior: dynamic problem

In dynamic problem:

*At equilibrium **acceleration** shall be considered:*

$$ES \frac{d^2 U(x,t)}{d_x^2} - \pi \tau_x D = \rho S \frac{d^2 U(x,t)}{d_t^2}$$

Where :

S: surface area of the nail section

E: young modulus of the steel

D:diameter of cross section

$$ES \frac{d^2 u(x,t)}{d_x^2} - \pi \tau_x D = \rho S \frac{d^2 u(x,t)}{d_t^2}$$

The main problem is that interface friction τ_x in case of dynamic loading is unknown

Identifying parameters influencing τ_x :

- Frequency
- Amplitude
- Confining pressure
- Soil properties

Aim of the Study:

Understanding
local interface
behavior

Identifying the
parameters on
which friction at
interface depends

?



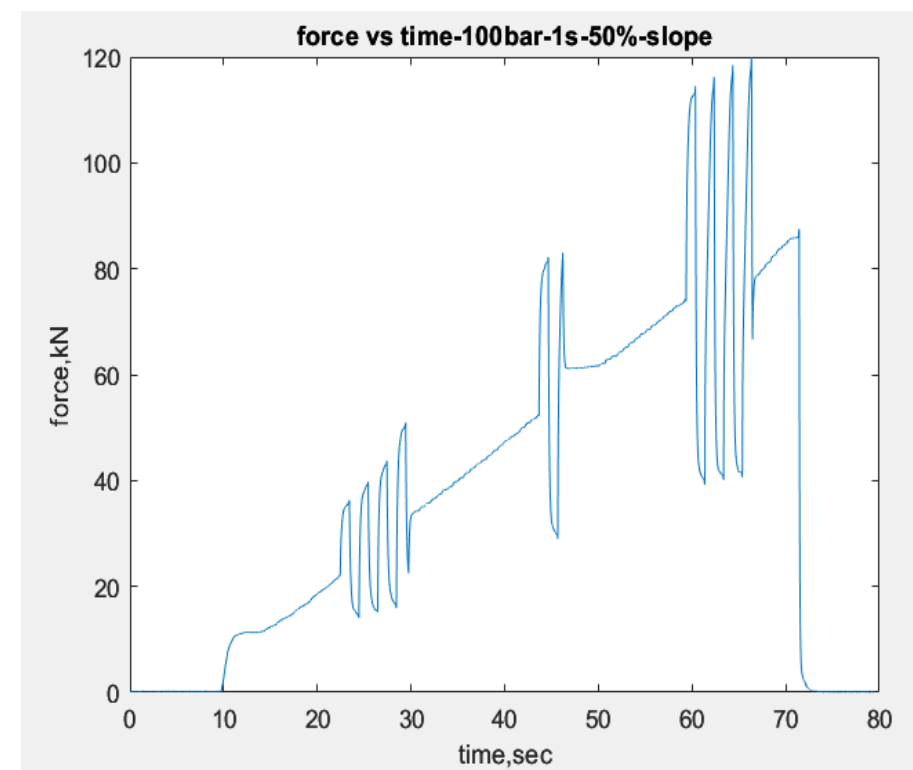
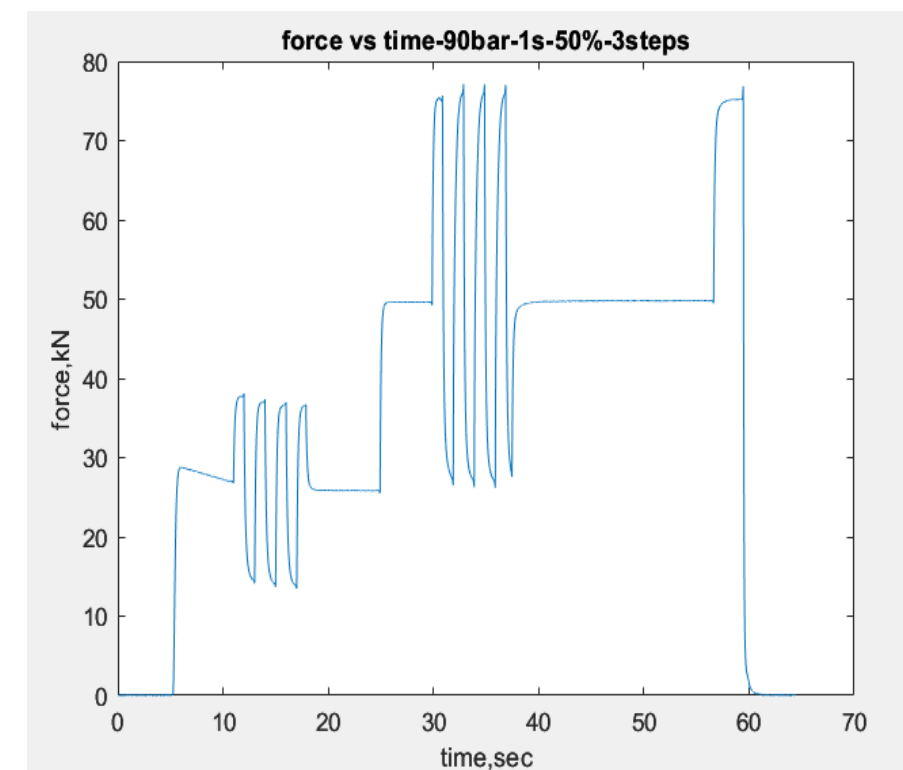
Through dynamic
pull-out tests.

The Dynamic pull-out device:

Operating Mode:

- Impose static tension load in two different configurations: incremental loading pullout tests (**steps configuration**) or during a linear increase of the tensile force (**slope configuration**).
- Superimposition of vibrational pulses centered around the static load with an amplitude at percentage of the static load (1-50% of the static tension).

Static Load		Dynamic pulse	
Duration	Magnitude	Frequency	amplitude



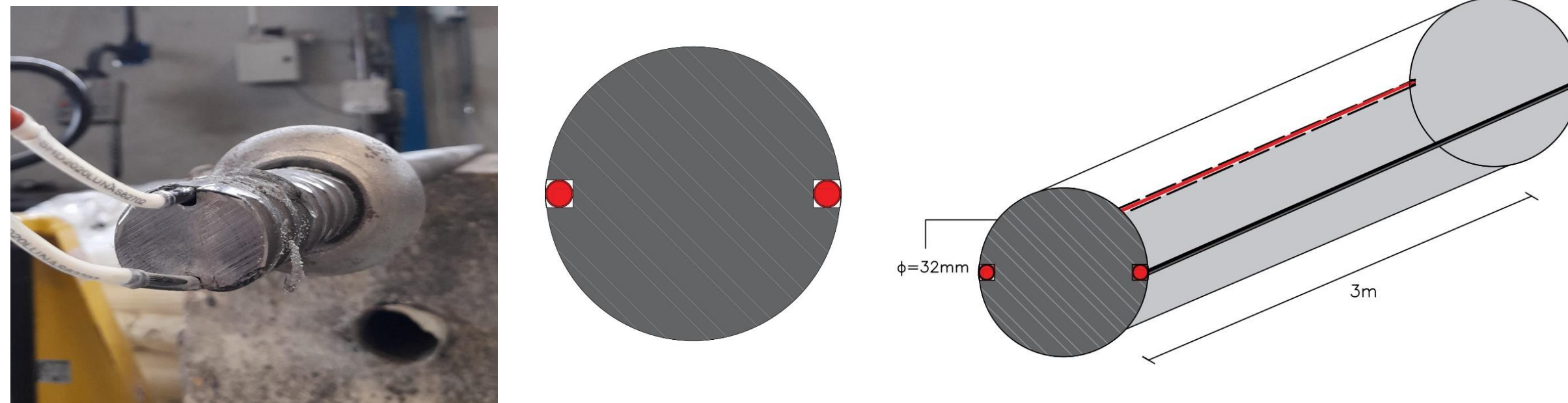
Hydraulic pump Hydraulic accumulator controlled solenoid valve programable automate (PLC)



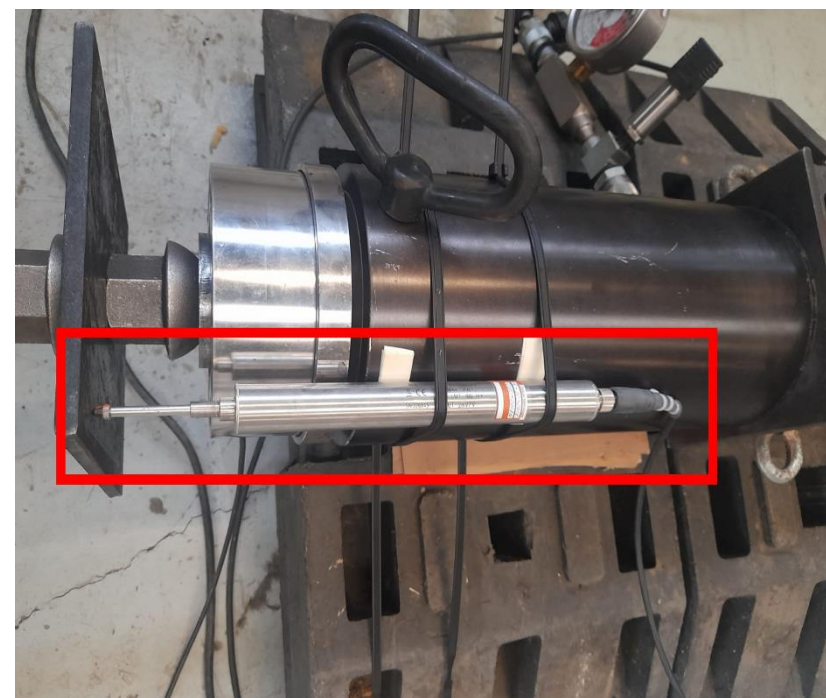
The dynamic pull-out device

Experimental Setup: connections and monitoring

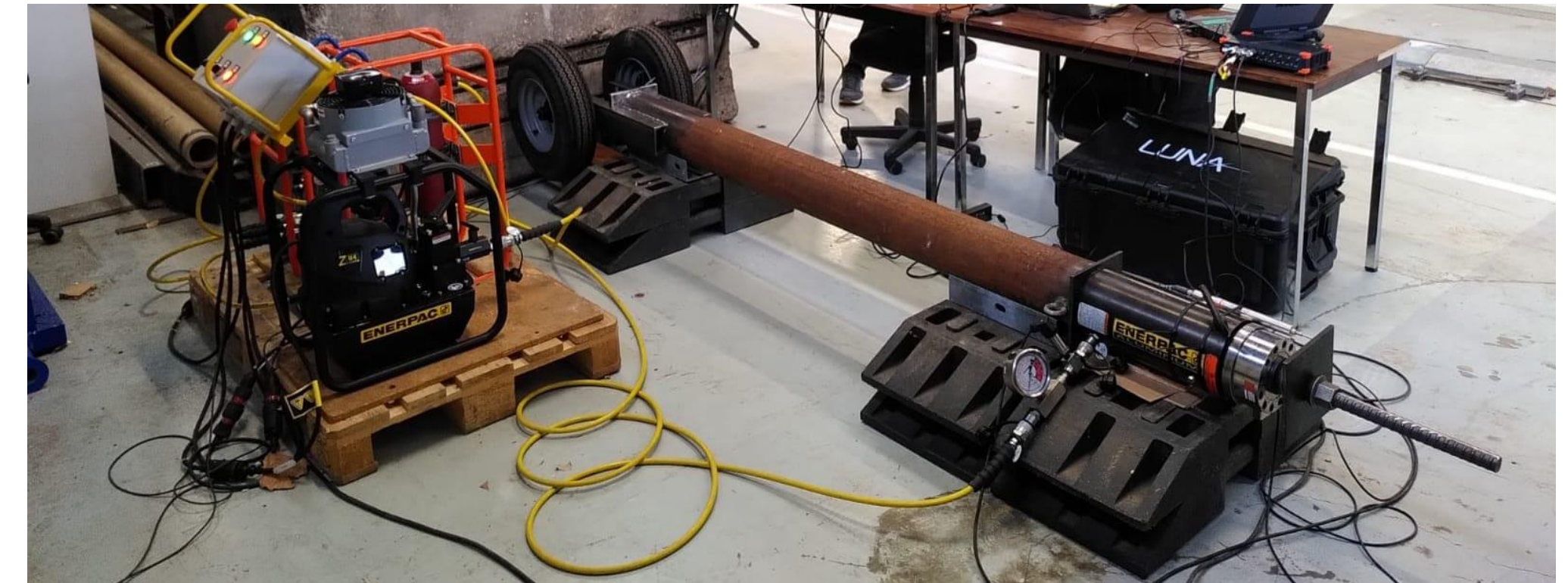
Connection of optical fiber along the steel bar:



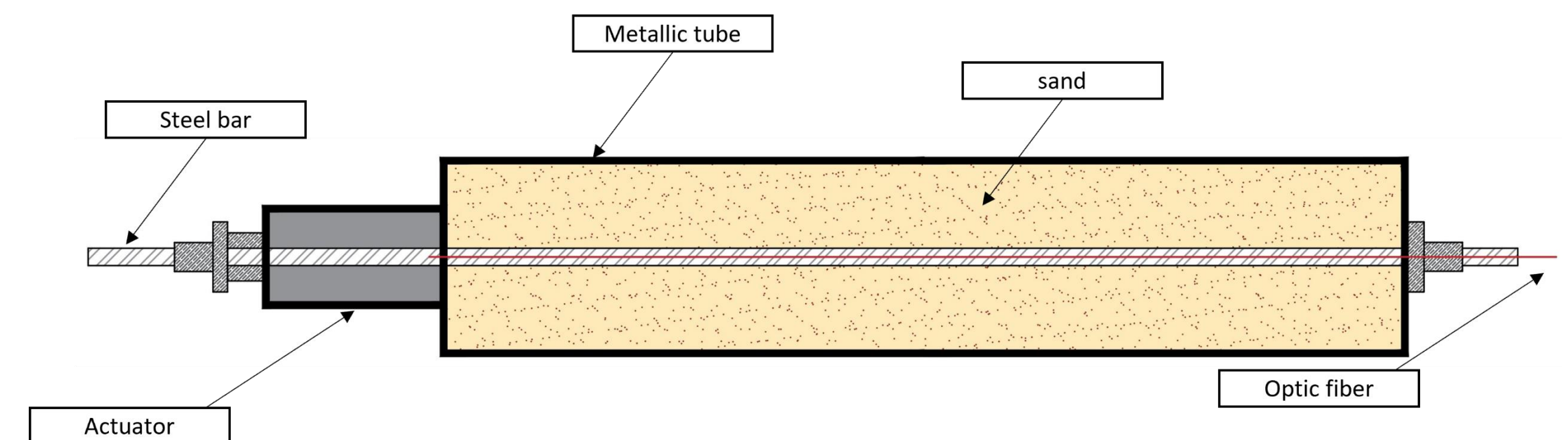
Double optical fiber connected along the two flat sides of the steel bar



Displacement and load sensors connected at the head of the nail

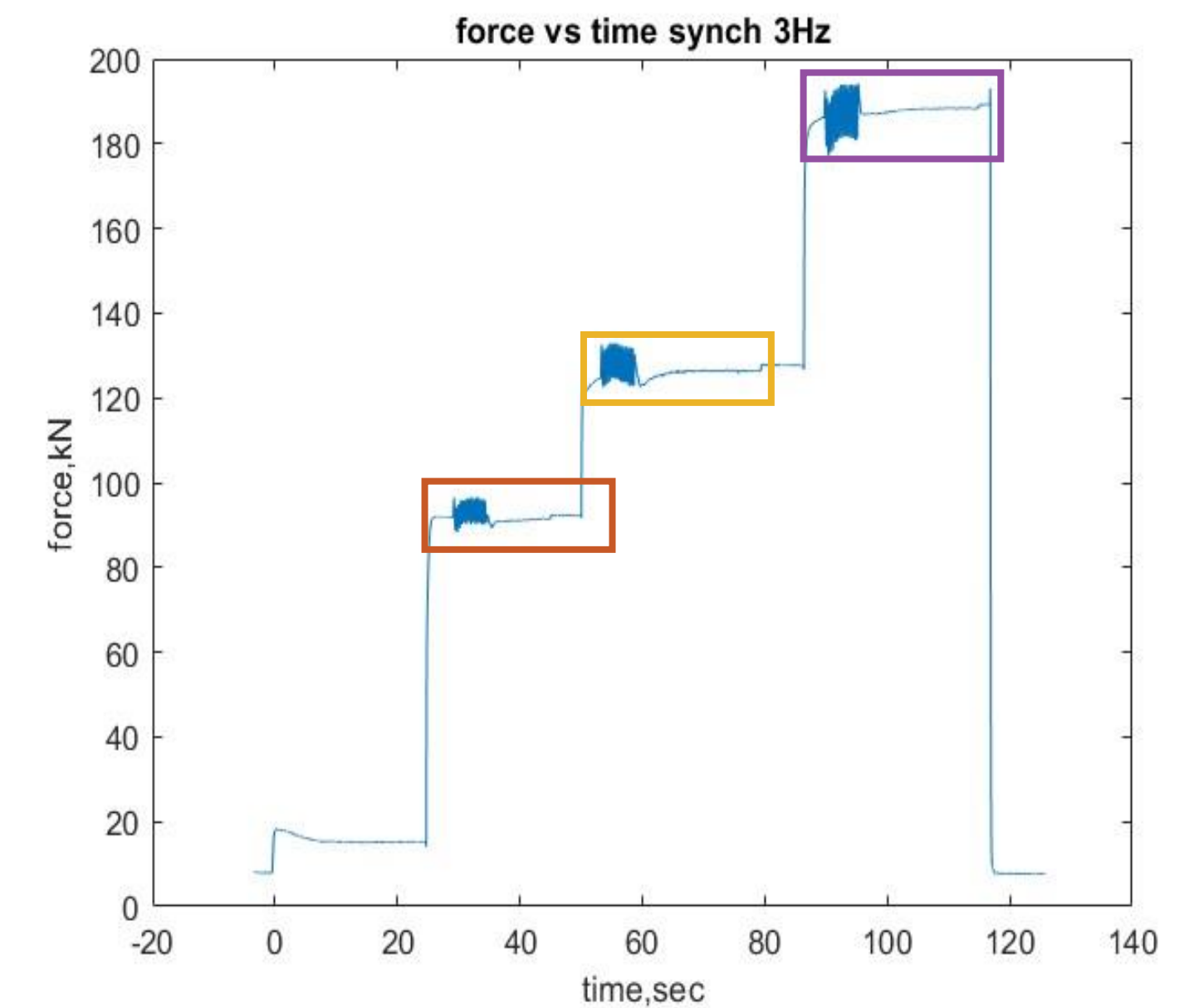


Employed setup connections



Test Protocol:

Test Name	Static load		Dynamic load (pulse)	
	Pressure(bar)	Duration (sec/step)	Amplitude(%)	Frequency(Hz)
Test0	10-100-140-213	30	-	-
Test 1-5%	10-100-140-213	30	5	1
Test 2-5%				2
Test 3-5%				3
Test 4-5%				4
Test 5-5%				5

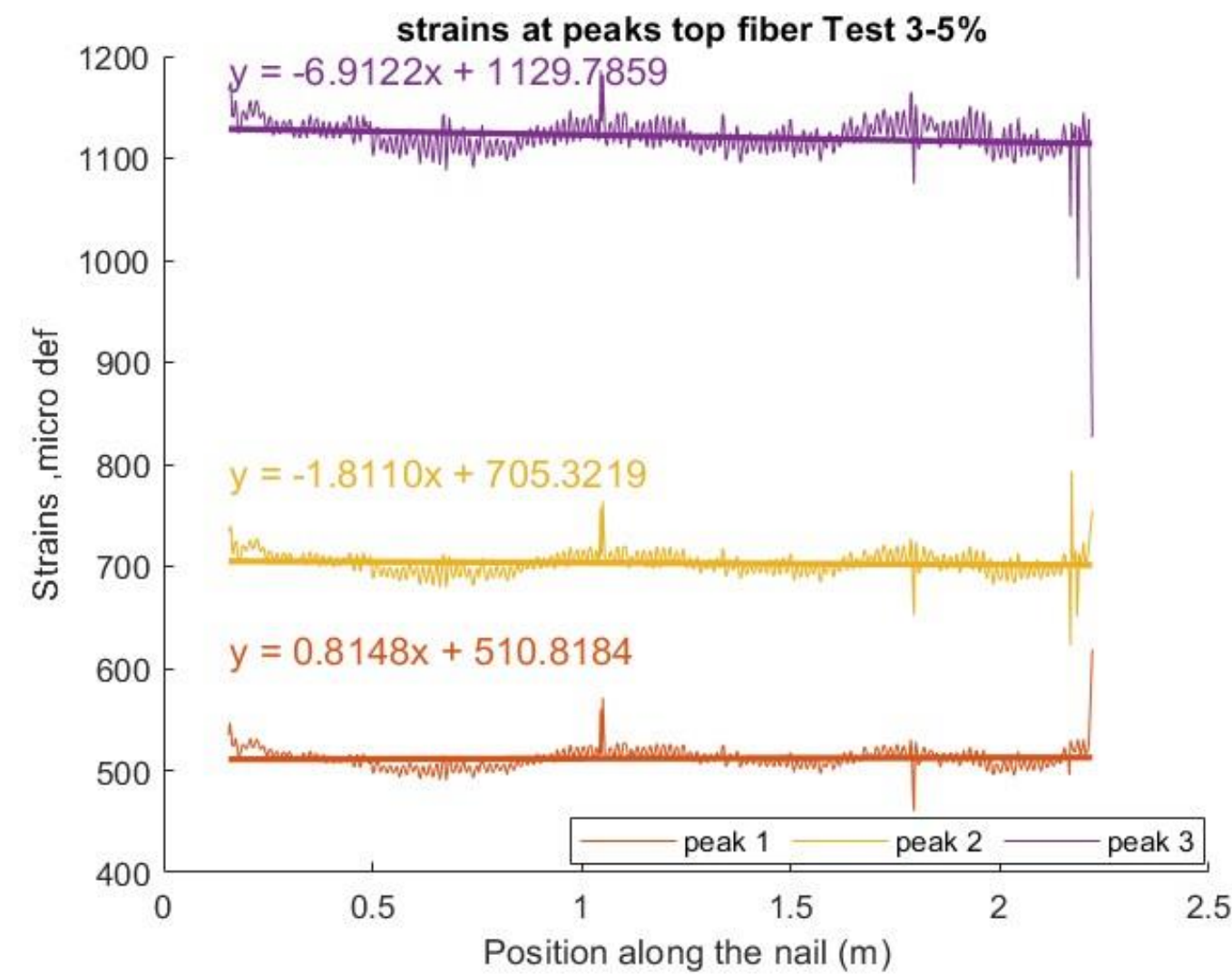


Pressure(bar)	10	100	140	213
Load(KN)	15,18	92	126	188

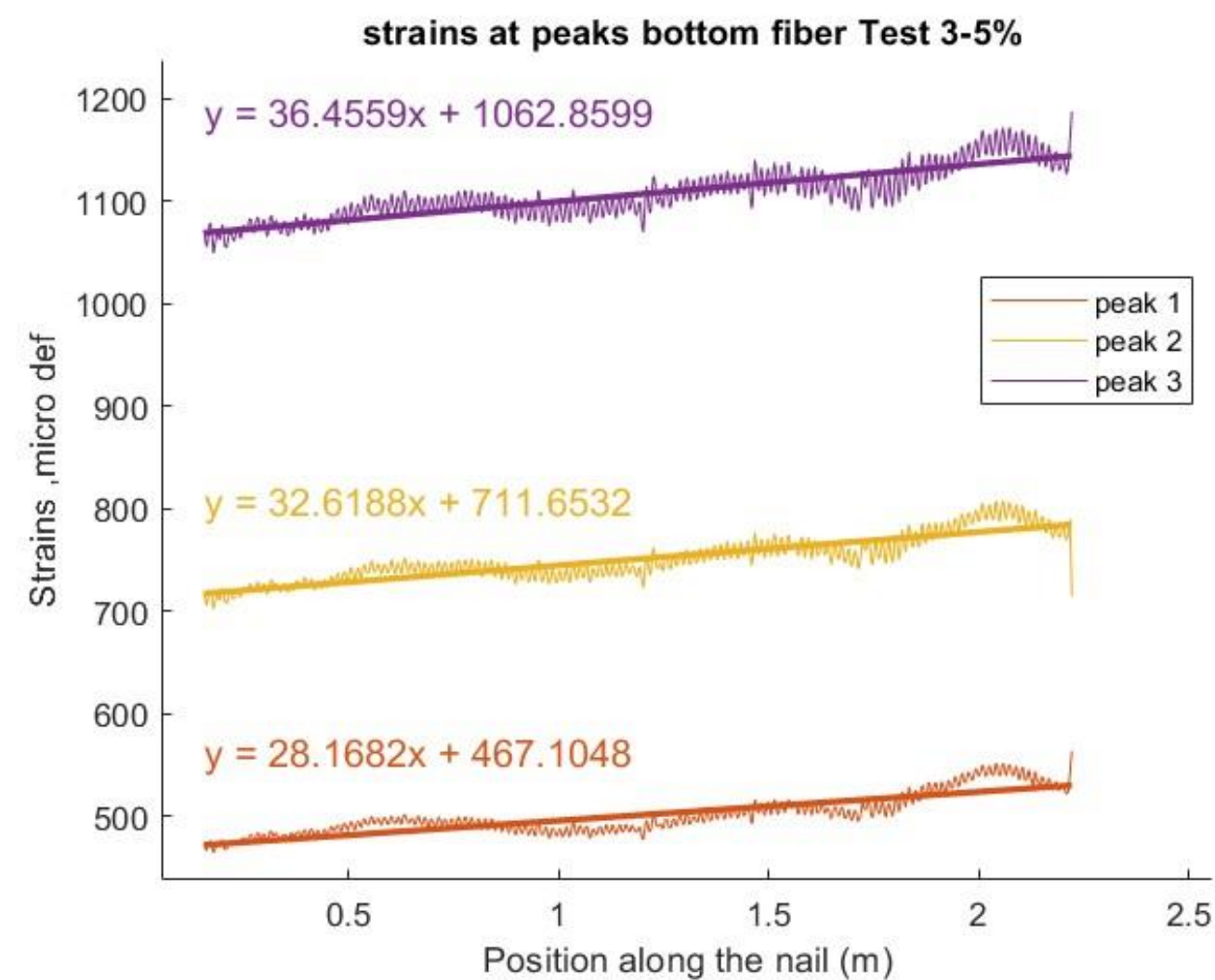
The duration of the pulse is **5sec** (manual timer is used)

Measured Strains: top vs bottom fiber

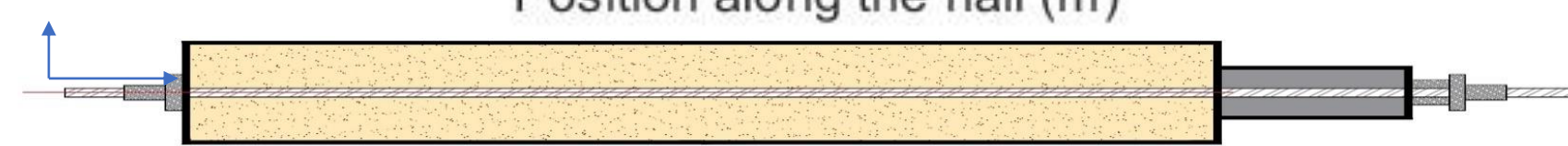
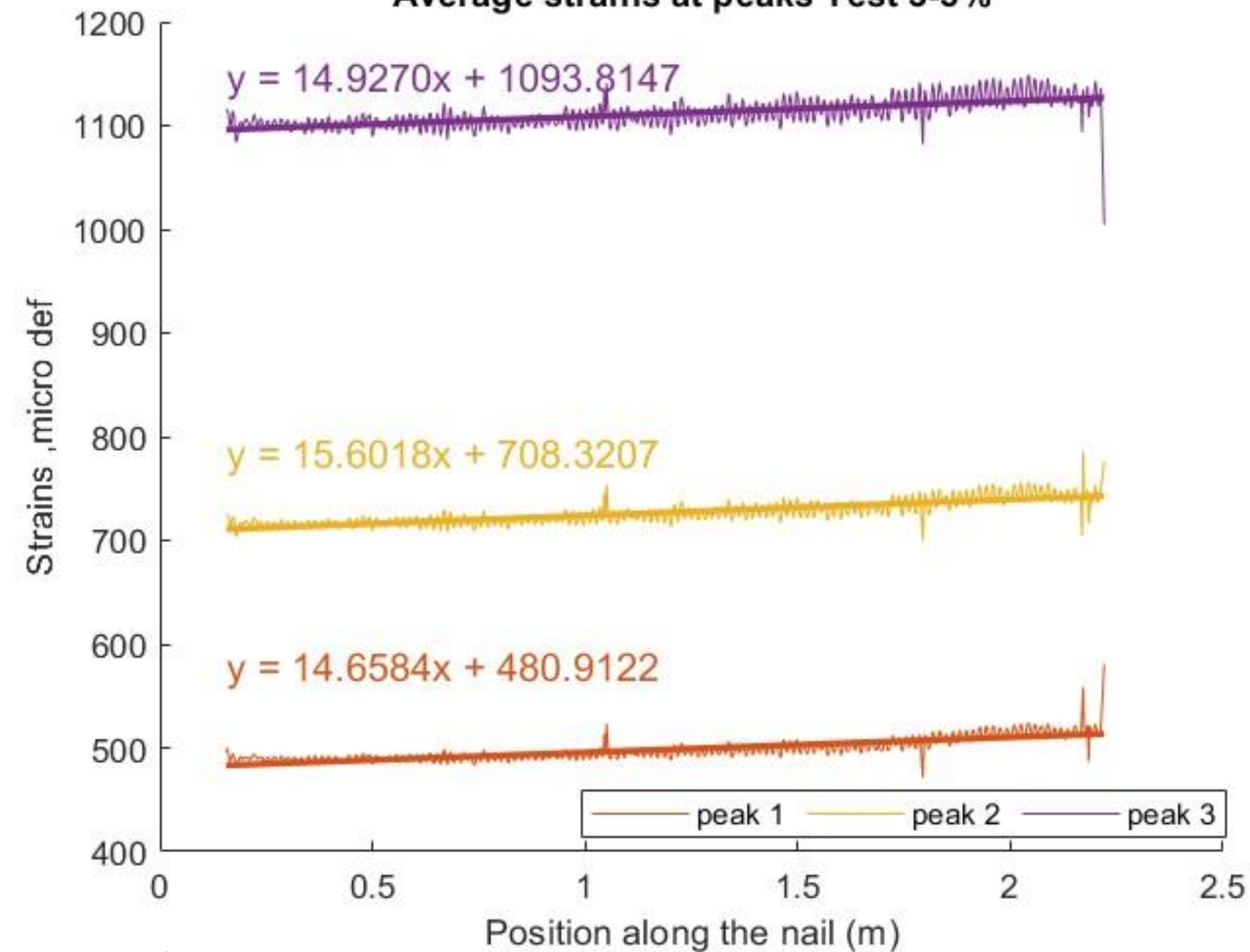
Test 3-5% Top fiber



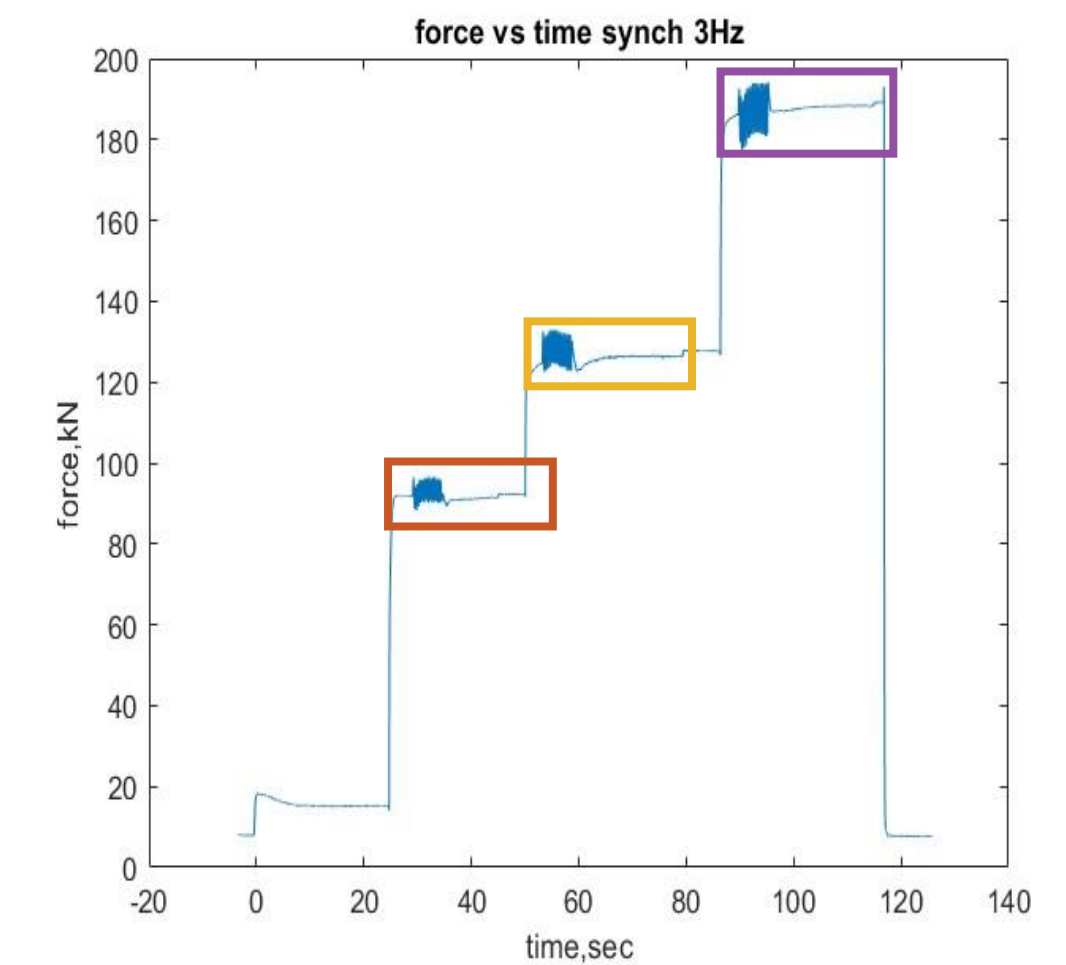
Test 3-5% Bottom fiber



Average strains at peaks Test 3-5%



Test 3-5% average of fibers

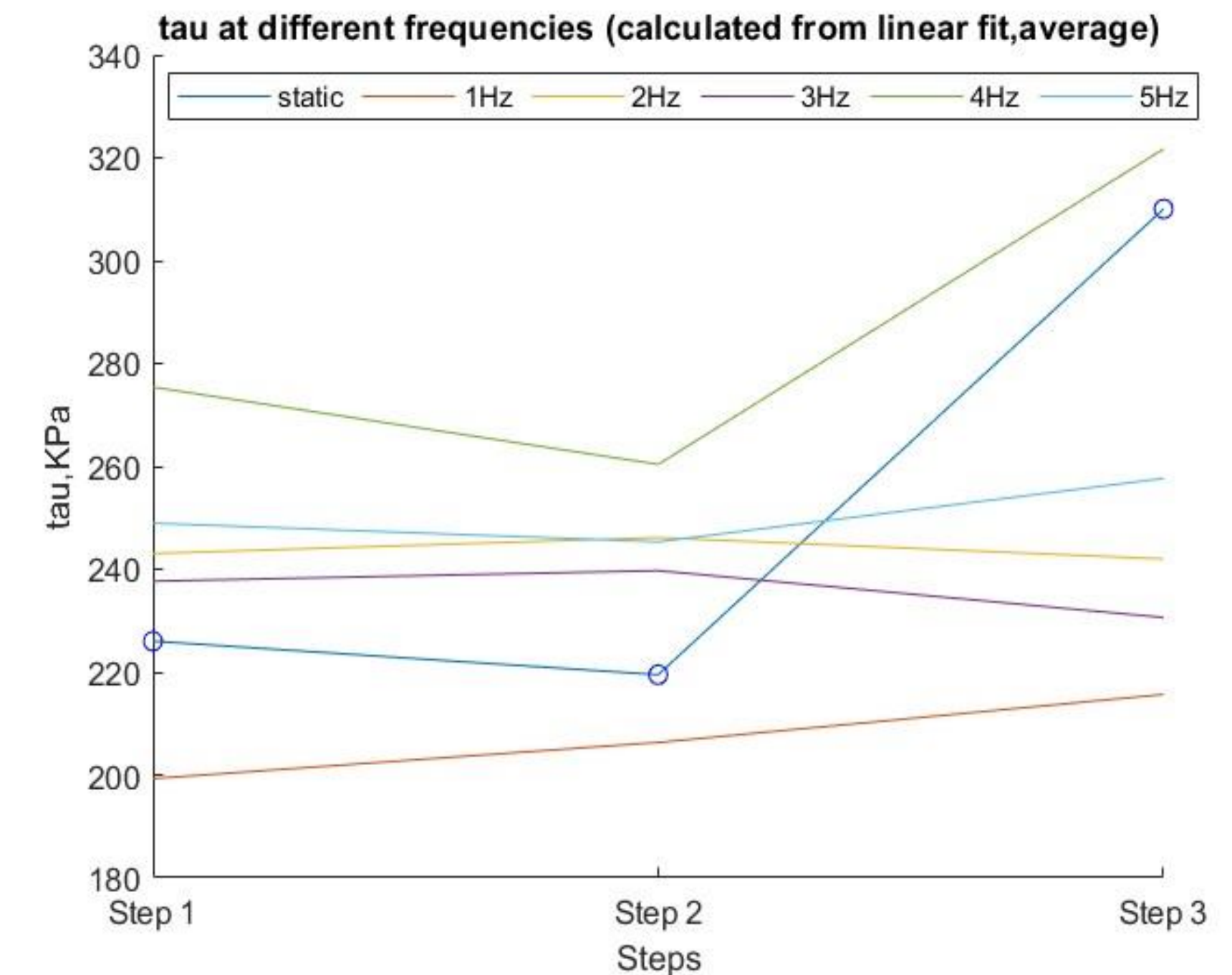
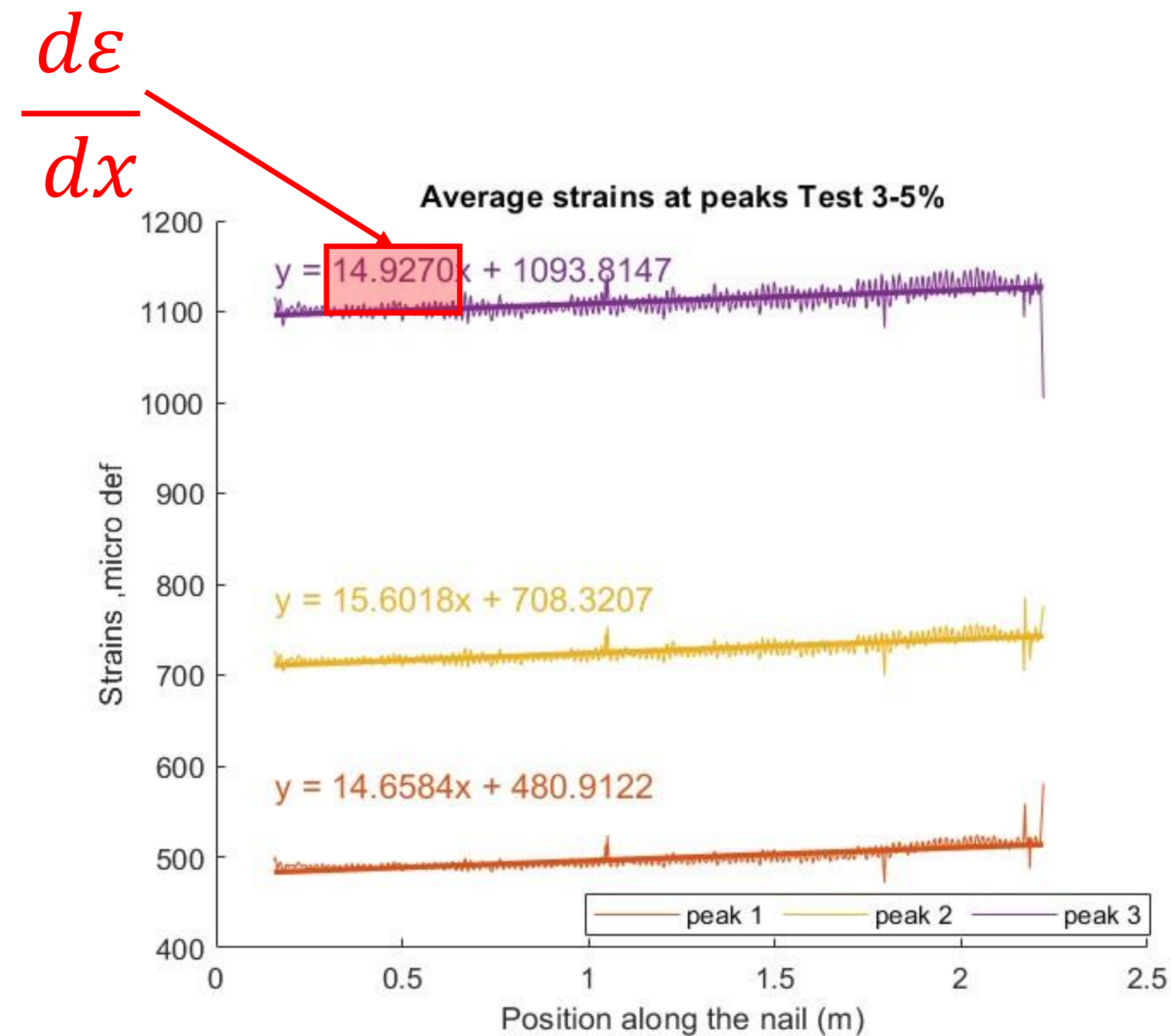


Evaluation of Interface friction coefficient τ :

- Tau(τ) is computed from **the linear fit** of strains at relative step and relative frequency, according to:

$$\tau = \frac{EA}{D\pi} \frac{d\varepsilon}{dx}$$

Where $\frac{d\varepsilon}{dx}$ is the slope of the linear fit.

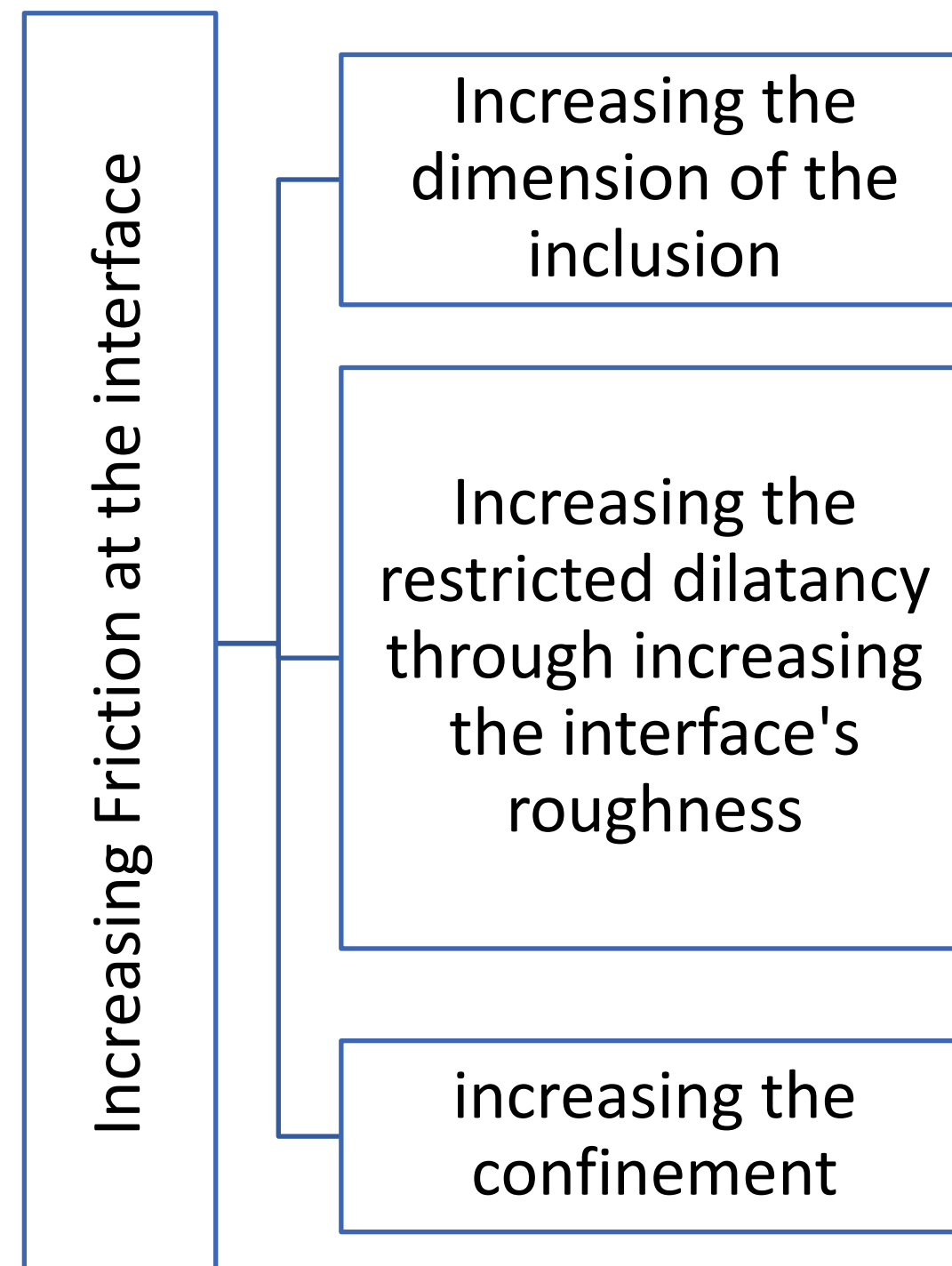


Average Strains

Increasing the Friction at interface: How?

$$F \sim \sigma \tan(\varphi) \frac{\pi d^2}{4}$$

The following equation allows us to see the factors influencing the friction force (F) occurring at the interface:



Increasing the Interface roughness:

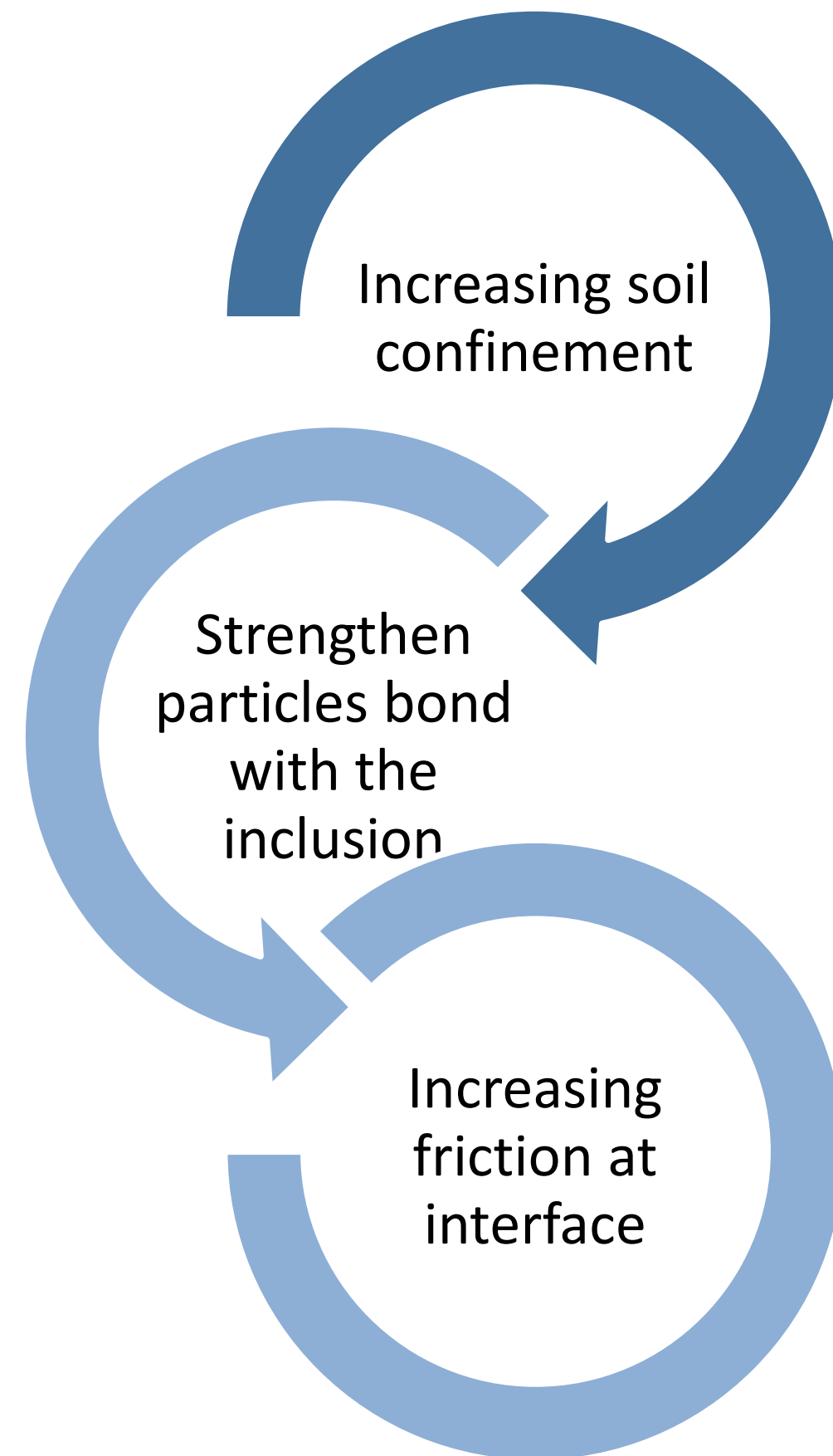
Grouting of the nail:

Sticking Sand particles to grout done in PVC (aid of glue).

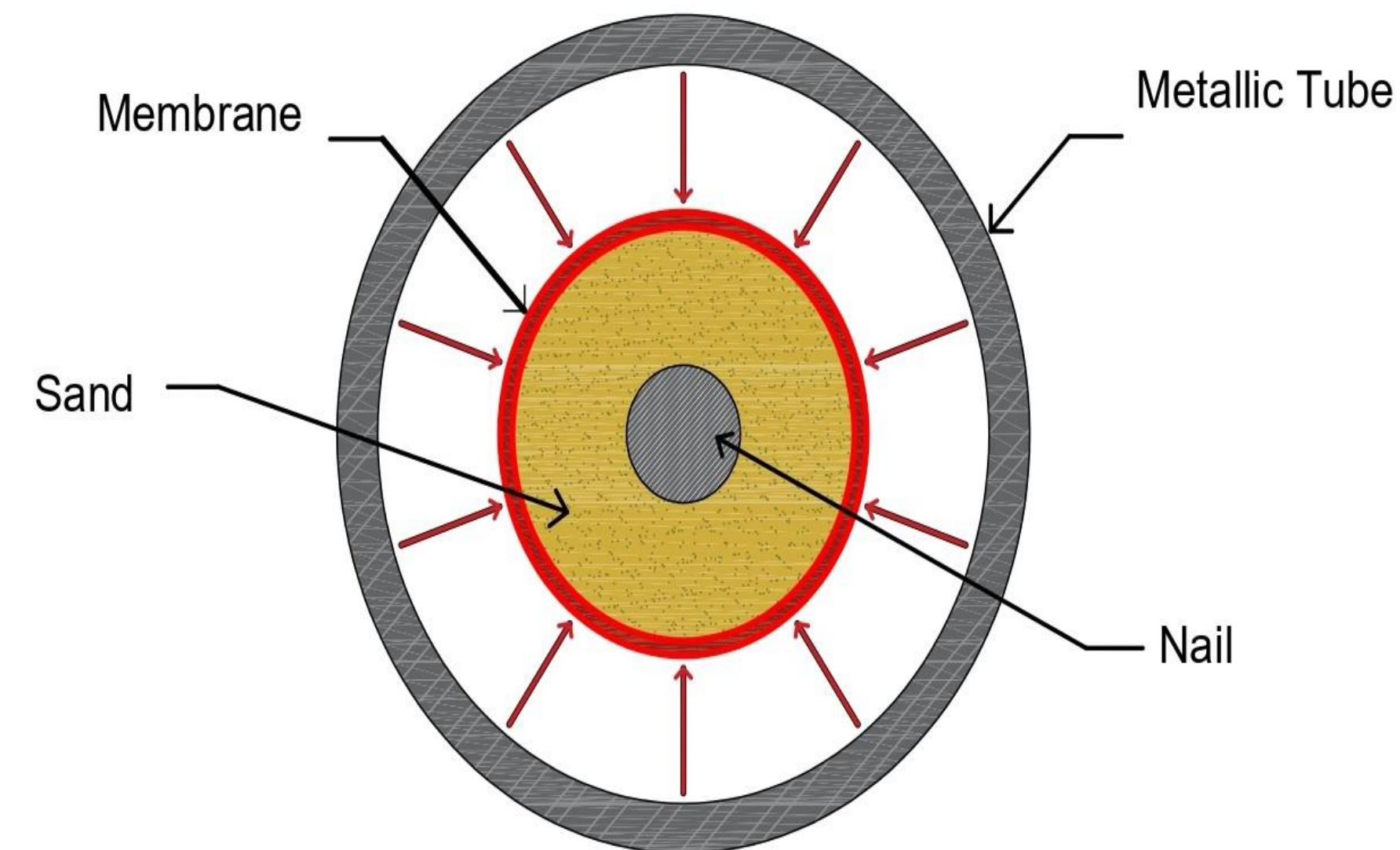
➤ W/C=0,45



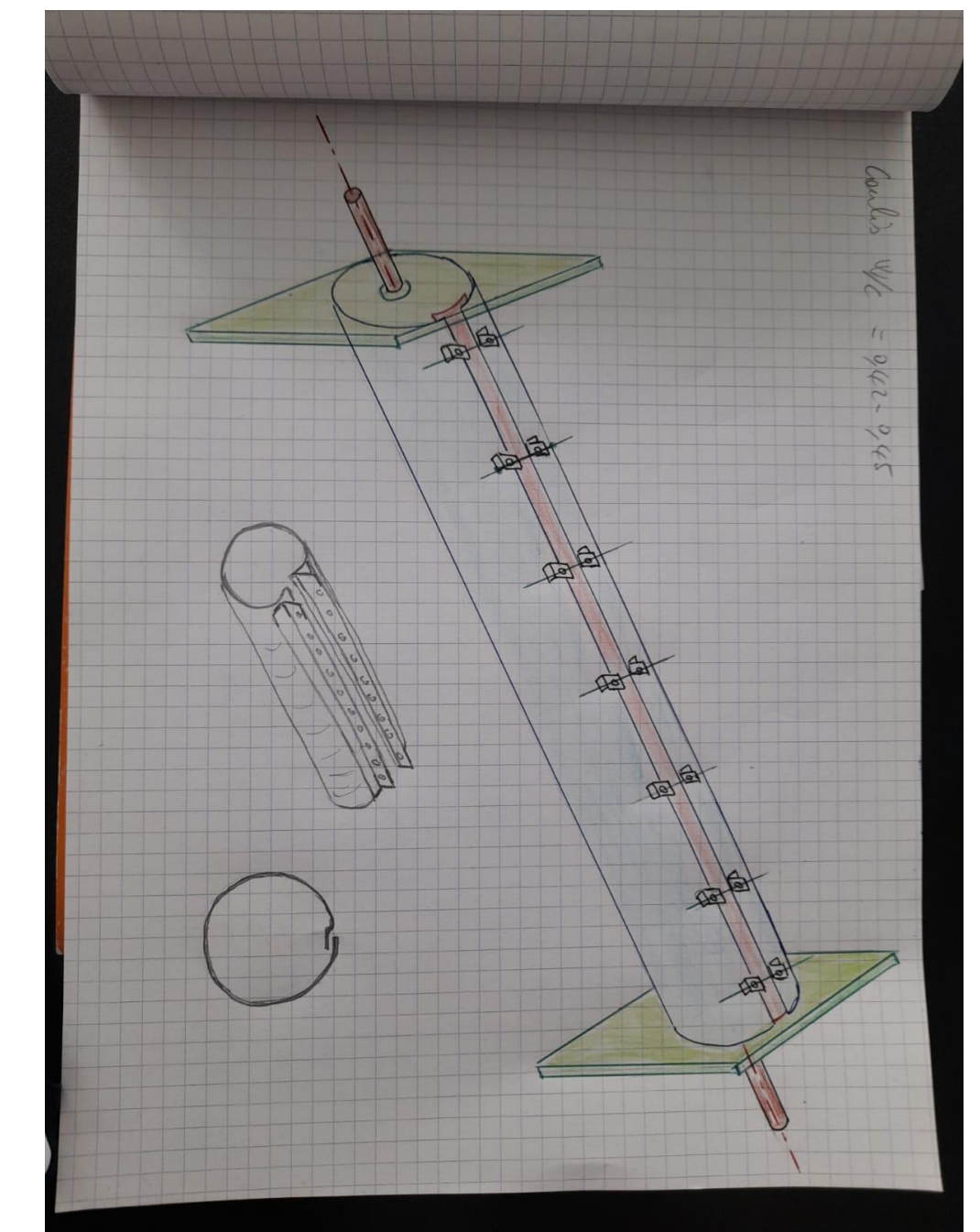
Increasing the Soil confinement:



Pressure application by fluid flow through an elastic membrane.



Adjustable compressible tube



Thank you for your attention



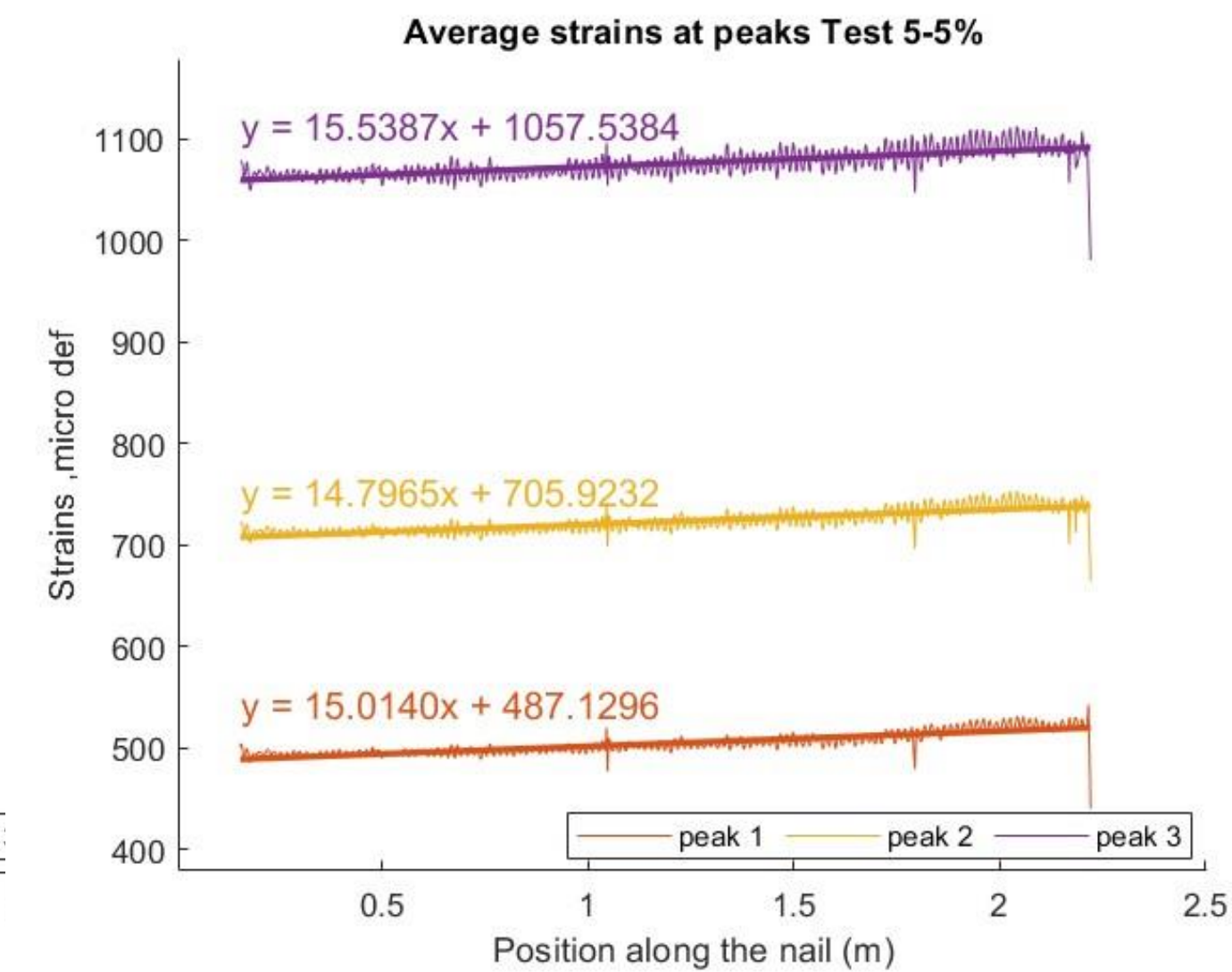
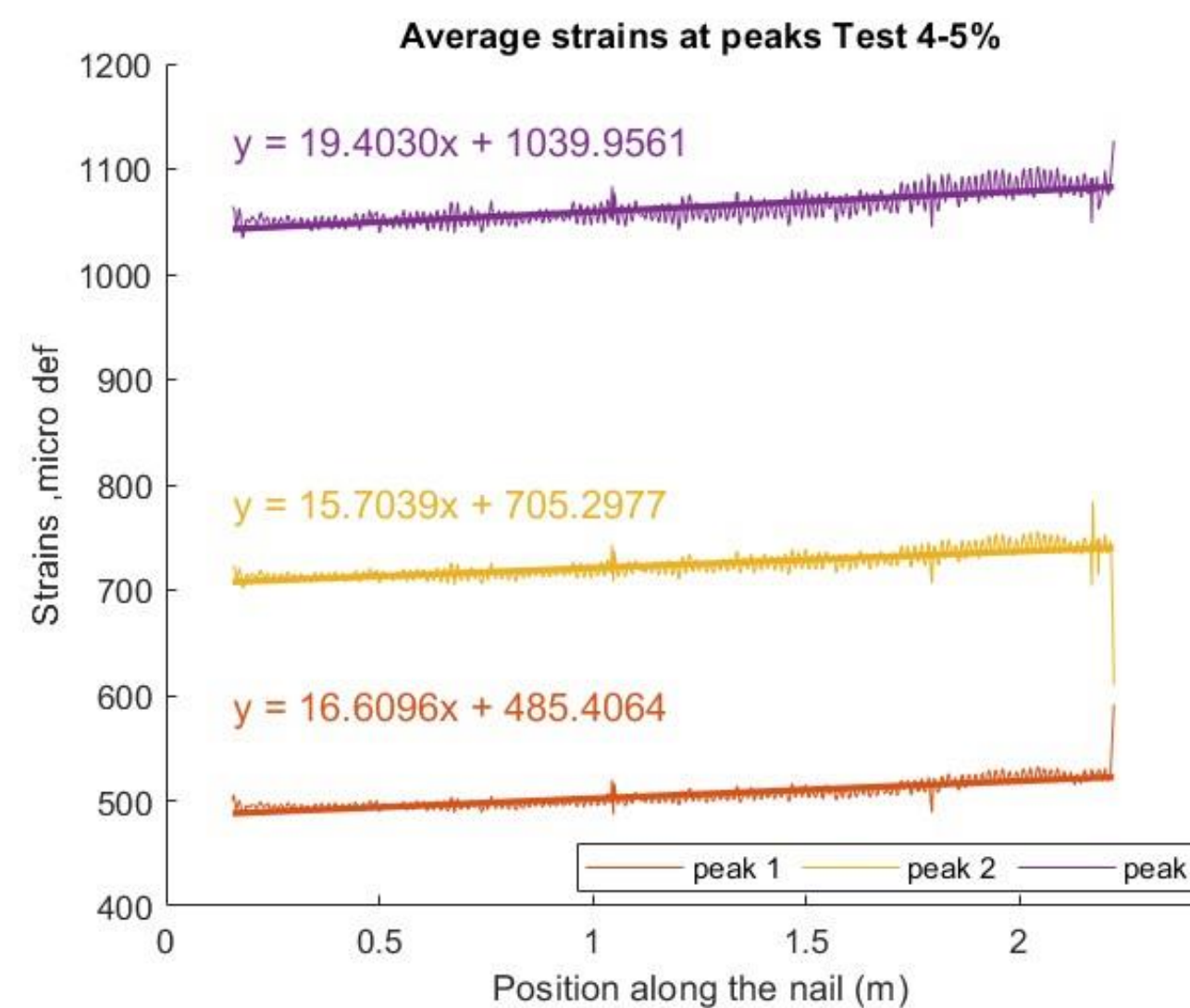
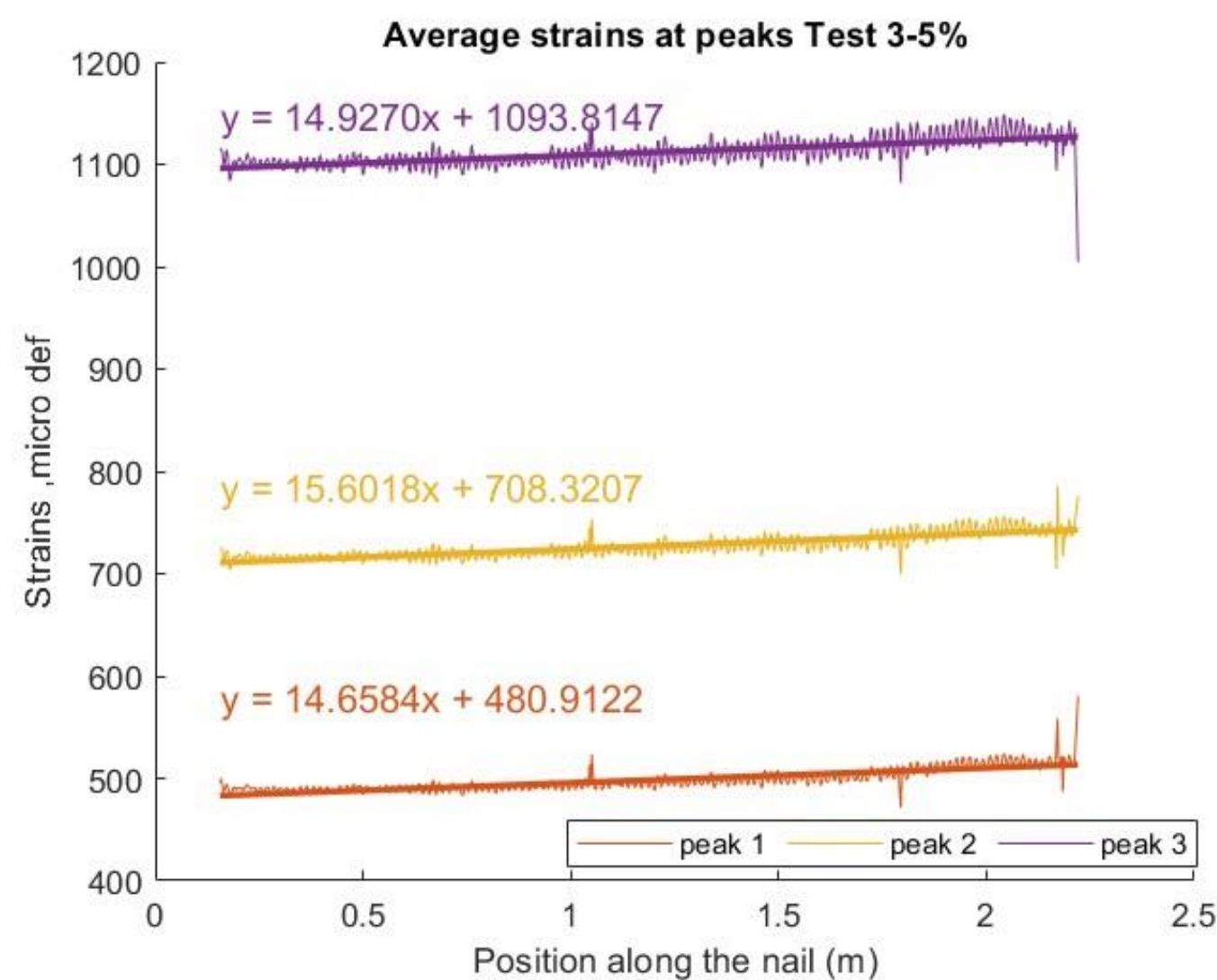
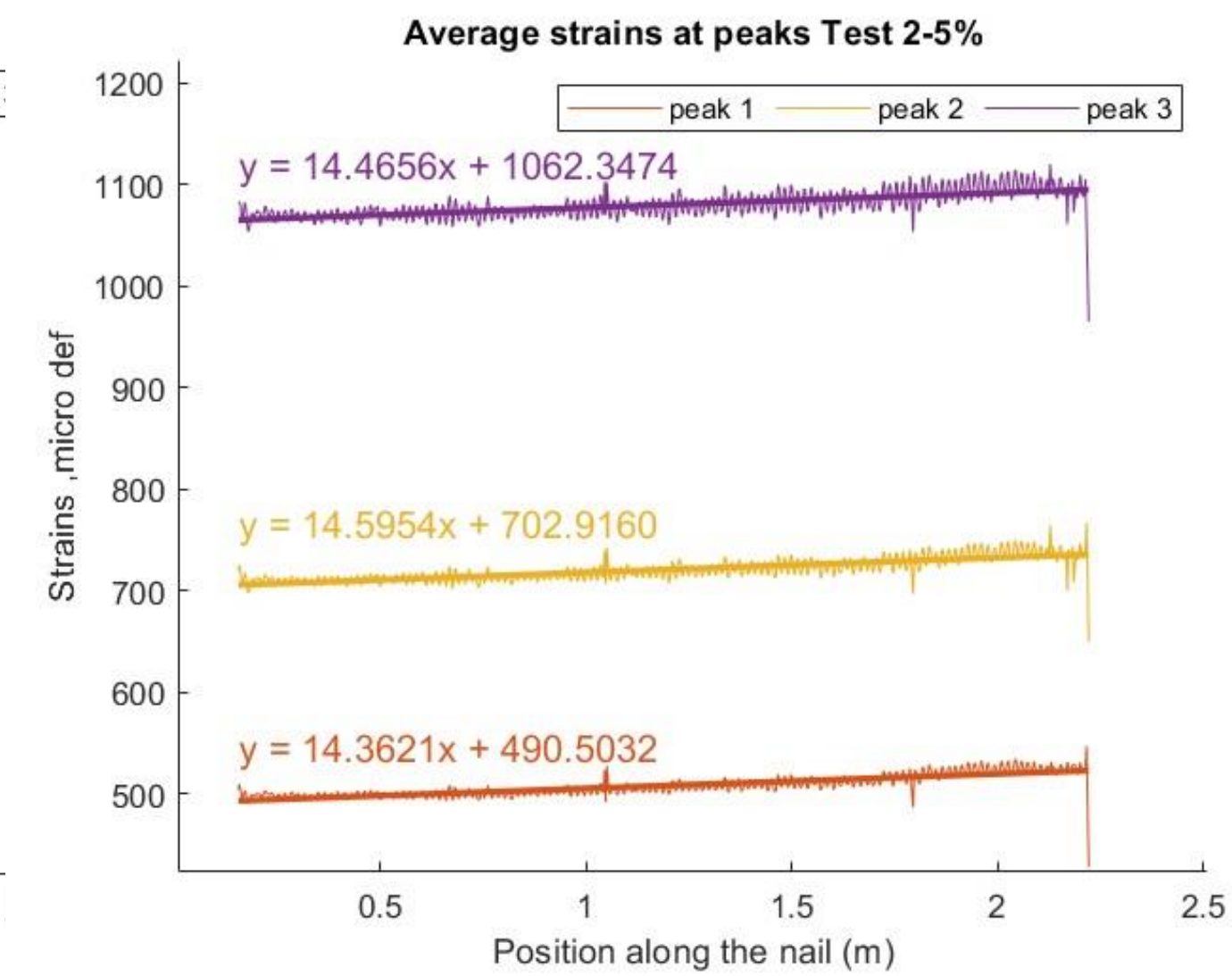
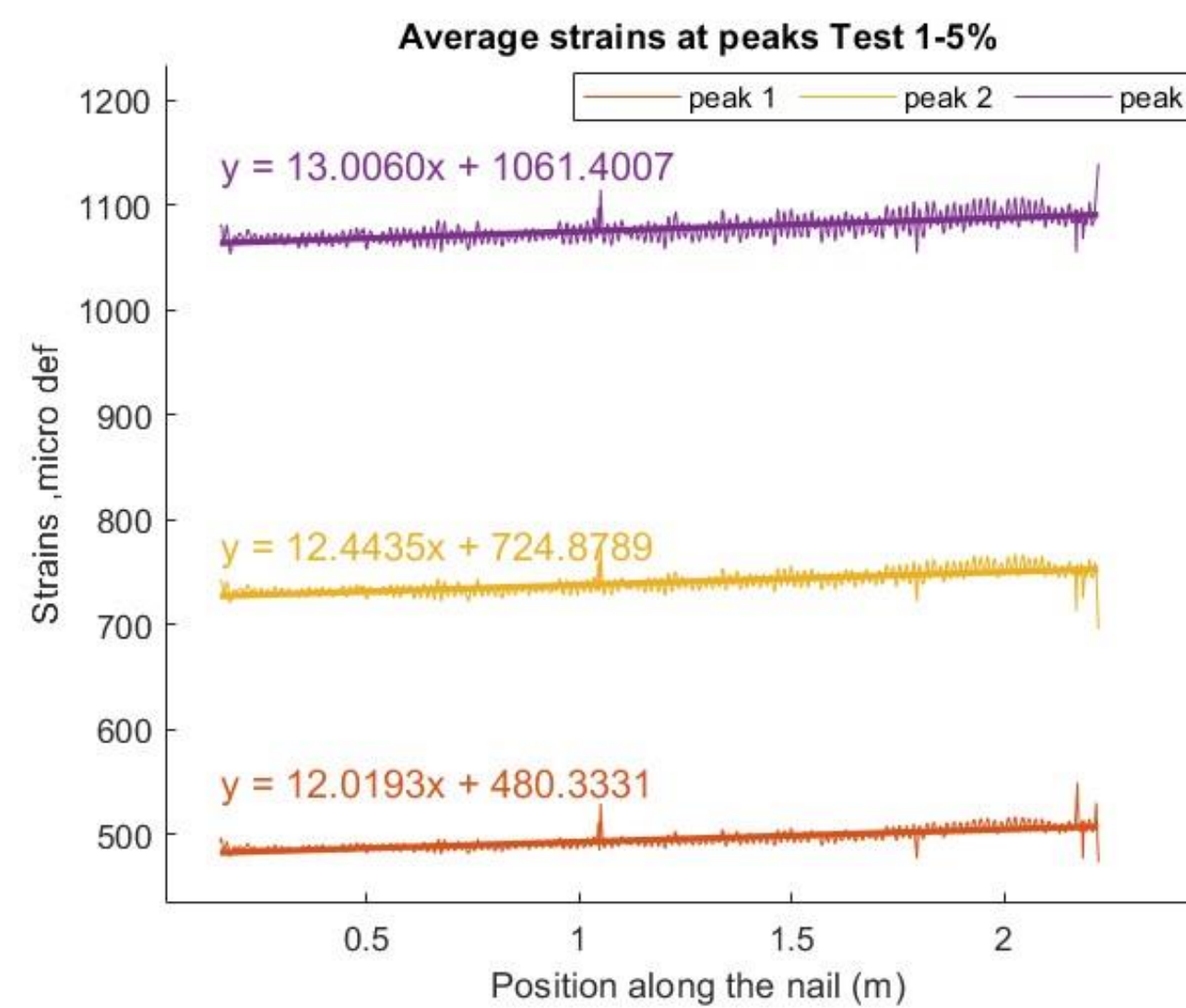
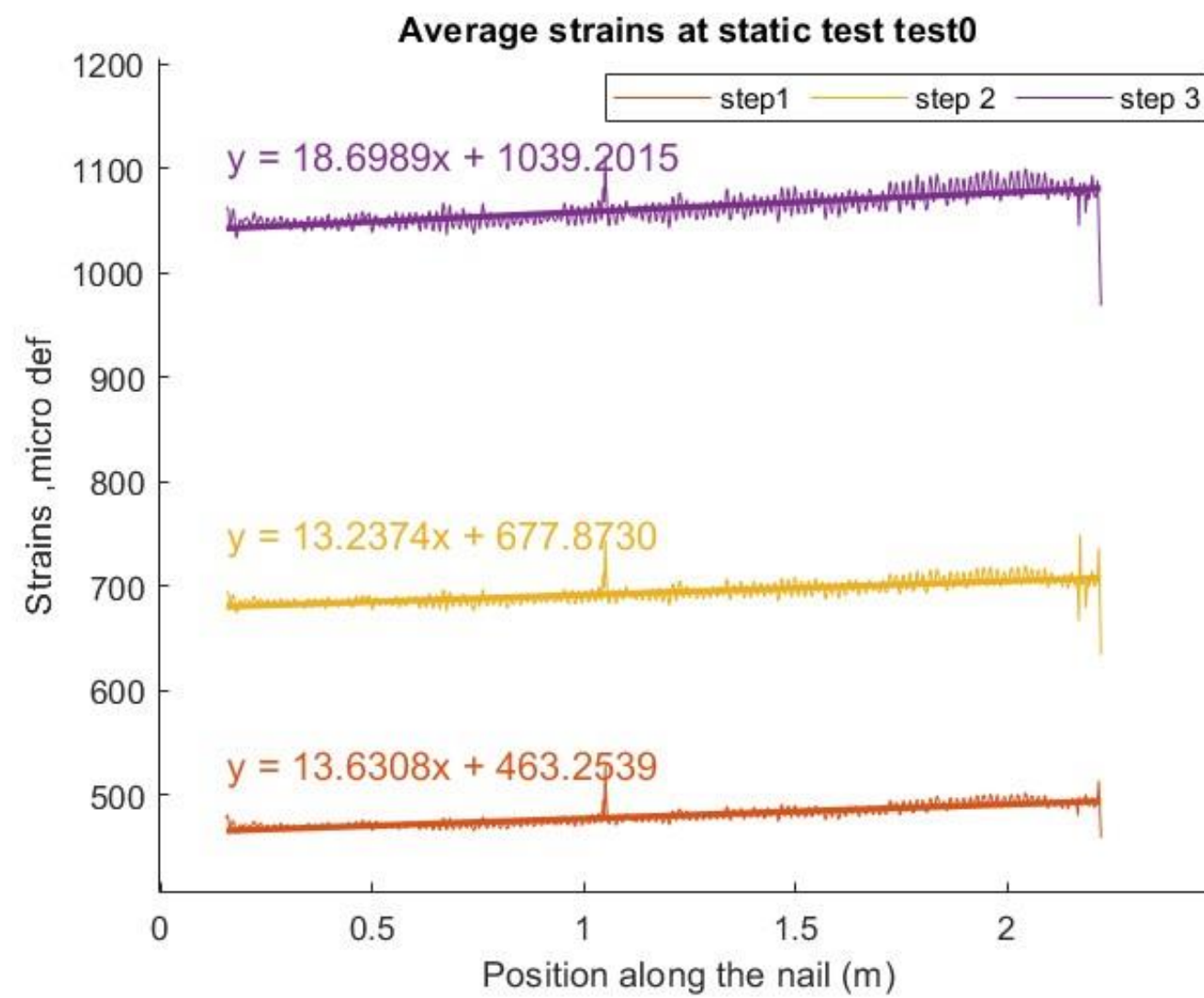
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Measured Strains: at different frequencies



Friction model proposed by FRANK and ZHAO:

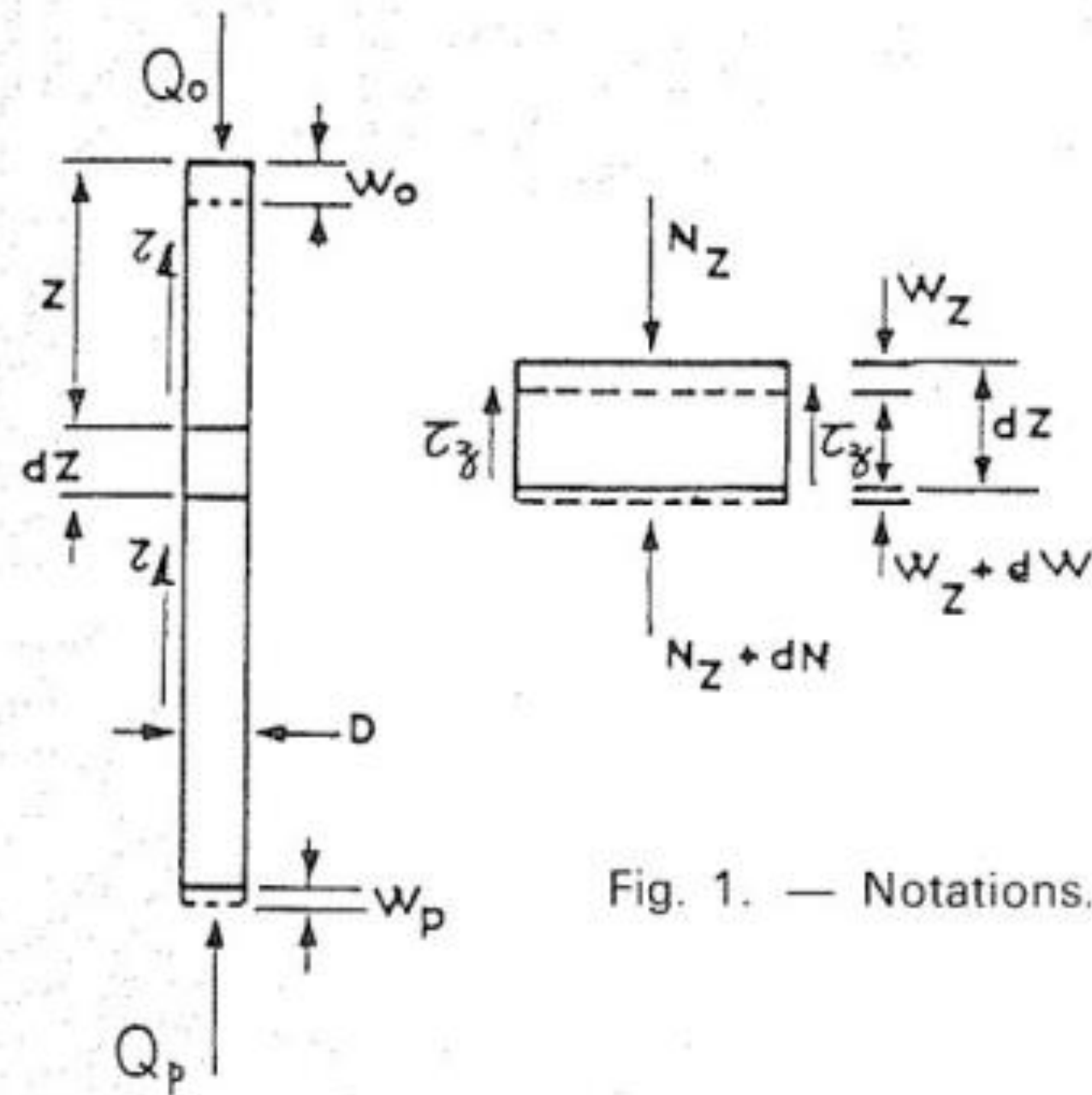


Fig. 1. — Notations.

